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Panel Ribs

23 Mar 1965

There are 11 ribs (Avg. of 22 Mar)

No	x' ft	WIDTH W ft	h^*	$l^{\dagger}$ (inches)	$\frac{.0417W}{h}$	$\frac{.2083W}{h}$	It is the distance from the plane of transverse curvature from the 20' member to the panel at rib center		
[1]	10.2 2.0	1.175 .95	4.5	1.342 16.10	.011	.054			
2	12.2 2.1	1.392 .91	4.1	1.559 18.71	.014	.070			
3	14.3 2.1	1.614 1.1	3.7	1.781 21.37	.013	.091			
[4]	16.4 2.2	1.831 1.27	3.6	1.998 23.98	.021	.106	1.789	1.704	1.664
5	18.4 2.0	2.033 1.42	3.5	2.200 26.40	.024	.121	1.988	1.891	1.866
6	20.4 2.2	2.231 1.58	3.4	2.398 28.78	.027	.137	2.183	2.073	2.064
[7]	22.4 2.5	2.425 1.65	3.5	2.592 31.10	.029	.144	2.375	2.260	2.258
8	24.9 2.8	2.662 1.71	3.7	2.829 33.95	.030	.150	2.611	2.491	2.495
9	27.3 2.8	2.885 1.75	3.9	3.052 36.62	.031	.154	2.833	2.710	2.718
10	29.7 1.3	3.102 1.72	4.3	3.269 39.23	.030	.151	3.051	2.930	2.935
11	31.0	3.218 1.70	4.5	3.385 40.62	.030	.149	3.167	3.048	3.051

* h is the distance, in the plane of transverse curvature, from the 20' member to the panel at rib center

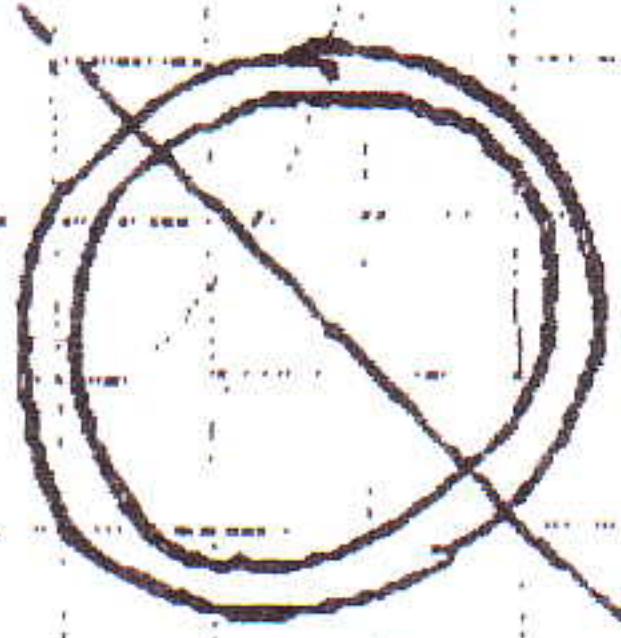
$\dagger l$ = length of blank = $W + 0.167$ ($2'' = 0.167$ ft)

x	y	$z + \frac{1}{12}$
1.143	1.100	1.008
1.357	1.301	1.225
1.575	1.503	1.447

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Angle versus tube

30 Mar 1965

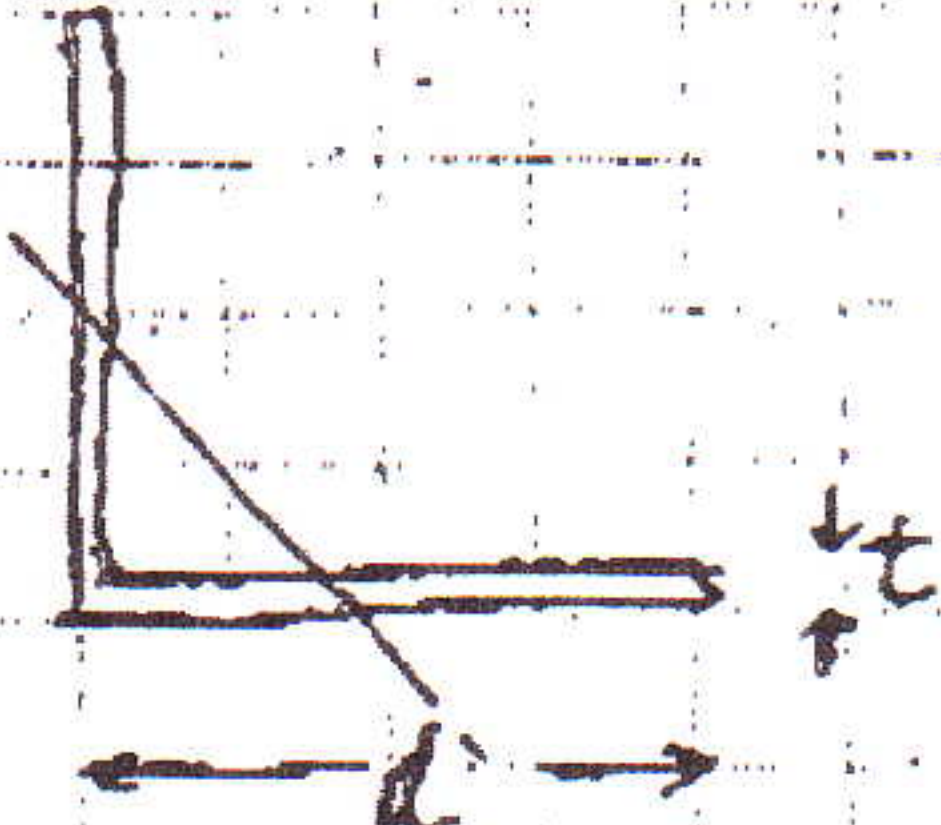


$$I_o = \frac{1}{2} \pi D t_o \frac{D^2}{4}$$

$$= \frac{\pi}{8} D^3 t$$

$$r \text{ of gyr} = \frac{\frac{1}{2} D}{\sqrt{2}}$$

$$= .7 \text{ radius}$$



$$I_L = 2 d t_L \left(\frac{d}{5} \right)^2 \quad (\text{thin section})$$

$$= \frac{1}{12} d^3 t$$

$$r \text{ of gyr} = \frac{d}{4\sqrt{6}} = \frac{d}{2\sqrt{6}}$$

For equal material, $\pi D t_o = 2 d t_L$

$$\frac{I_o}{I_L} = \frac{3 \pi D t_o}{d^2 t_L} = \frac{12}{\pi} = 16 \quad 1.2$$

For equal weights, $\frac{I_o}{I_L} = 16$ tube has 16 times more moment of inertia than angle.

Tube Equivalent Angle r. of gyr

$1\frac{1}{4}" \text{ d.}$	2.5×2.5	.44"
	2.0 x 2.0	
	2.3×2.3	
$1\frac{1}{4}" \times .049$	2.0 x 2.0 .063	

From tables

Calc

	r	area	I	
O $1\frac{1}{4}" \times \frac{1}{16}"$	.42	.233	.041	area = $\pi \times 1\frac{1}{4} \times \frac{1}{16} = .24$ gyr = $.07 \times \frac{1}{8} = .44$
L $2 \times 2 \times \frac{1}{16}$	.4	.25	.04	area = .24 gyr = $2/50 = .4$

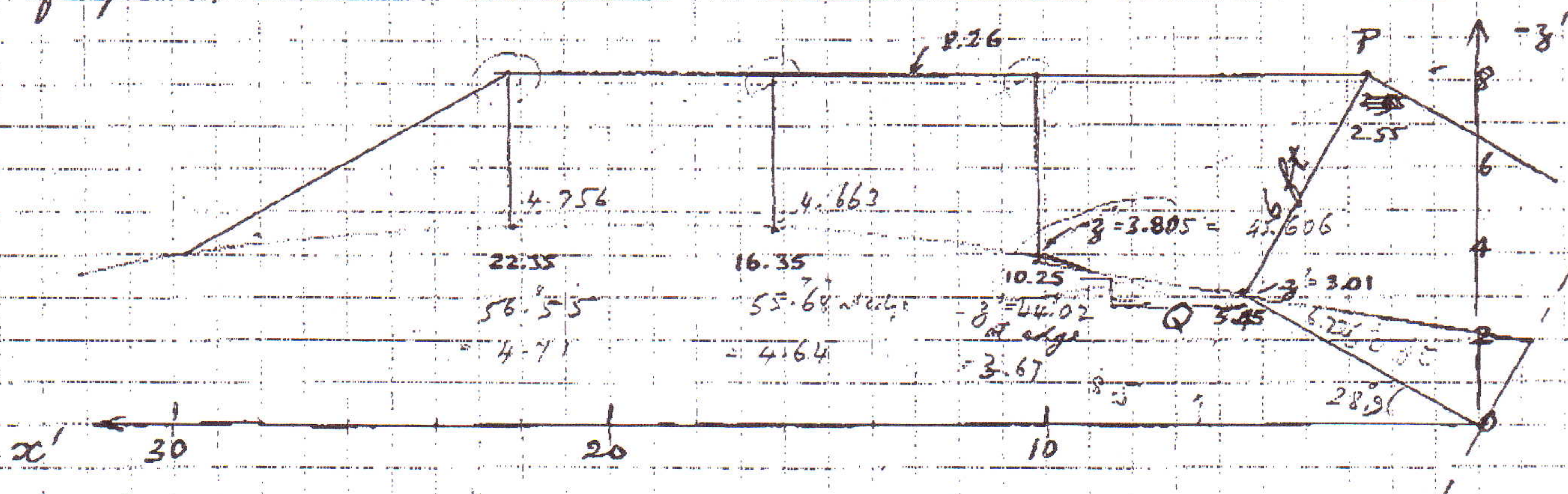
Tests (p. 31) show that $2 \times 2 \times .063$ angle is too thin and fails before developing calculated strength. Thin walled tube $1\frac{1}{4}"$ dia $\times .049$ is OK however

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Fixing Spine Location

Apr 6 1965

From Dwg No. RC-124 adopt $-z' = 8.26$ feet for location of spine.



Location of main ribs, from Dwg: $x' = 10.25, 16.35, 22.35$

To locate points P and Q: Assume $PQ = 6$ ft., angle is 28.9°

$$\begin{aligned} \text{Then } -z'_Q + 6 \cos 28.9 &= 8.26 \\ x'_Q &= -z'_Q \cot 28.9 \\ x'_P &= x'_Q - 6 \sin 28.9 \end{aligned} \quad \left. \begin{aligned} -z'_Q &= 3.01 \\ x'_Q &= 5.45 \\ x'_P &= 2.55 \end{aligned} \right\}$$

The accuracy is about ± 0.01 ft and depends on the 6 ft. dimension, which is still open to change. The 8.26 dimension is effectively frozen by this decision.

$$6.22 \cos 28.9 = 5.45$$